

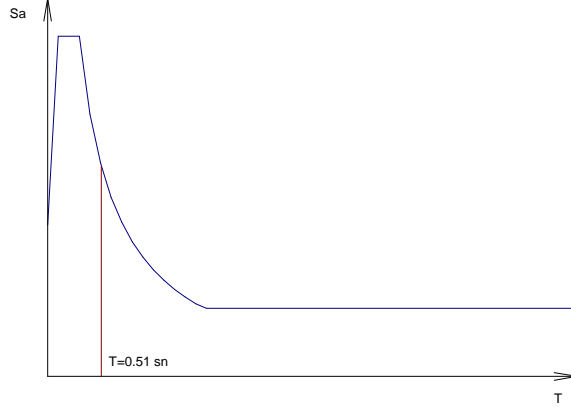
DEPREM RAPORU

DEPREM STANDARDI : TDY2006 CODE
 Deprem yükü eksantirisitesi : 0.050
 DIYAFRAM SAYISI : 9
 Diyafram tanımı : KAT(diyafram no)
 Dinamik Analiz min. deprem yükü oranı β : 0.9
 YAPI DAVRANIŞ KATSAYISI : 8.00

DİNAMİK ANALİZ BİLGİLERİ

TASARIM SPECTURUM BİLGİSİ (TDY97 SPECTRUM)

T (s)	Sa (m/s ²) Ao.I.S (t)
0.00	4.000
0.10	10.000
0.30	10.000
0.40	7.944
0.50	6.644
0.60	5.744
0.70	5.076
0.80	4.564
0.90	4.152
1.00	3.816
1.10	3.536
1.20	3.300
1.30	3.096
1.40	2.916
1.50	2.800
5.00	2.800



MODAL ANALİZ - YAPI PERYOD ve VEKTORLERİ

Mod w T yön	1.mod 12.31 0.5103 y	2.mod 12.41 0.5064 b	3.mod 12.67 0.4960 x	4.mod 12.68 0.4954 x	5.mod 15.61 0.4026 b	6.mod 15.62 0.4024 y	7.mod 38.36 0.1638 y	8.mod 38.66 0.1625 b	9.mod 39.32 0.1598 x
1/1x	0.00000	0.00000	0.00103	0.00000	0.00000	0.00000	0.00000	0.00000	0.00327
2/2x	0.00000	0.00000	0.08894	0.08841	0.00000	0.00000	0.00000	0.00000	0.24312
2/3x	0.00000	0.00000	0.08894	-0.08841	0.00000	0.00000	0.00000	0.00000	0.24312
3/4x	0.00000	0.00000	0.19046	-0.19024	0.00000	0.00000	0.00000	0.00000	0.28777
3/5x	0.00000	0.00000	0.19046	-0.19024	0.00000	0.00000	0.00000	0.00000	0.28777
4/6x	0.00000	0.00000	0.26915	0.26921	0.00000	0.00000	0.00000	0.00000	0.02925
4/7x	0.00000	0.00000	0.26915	-0.26921	0.00000	0.00000	0.00000	0.00000	0.02925
5/8x	0.00000	0.00000	0.31369	0.31393	0.00000	0.00000	0.00000	0.00000	-0.26877
5/9x	0.00000	0.00000	0.31369	-0.31393	0.00000	0.00000	0.00000	0.00000	-0.26878
1/1y	0.00310	0.00000	0.00000	0.00000	0.00000	0.00007	0.00998	0.00000	0.00000
2/2y	0.09230	-0.08982	0.00000	0.00000	-0.00007	-0.00007	0.24863	-0.24421	0.00000
2/3y	0.09230	0.08982	0.00000	0.00000	0.00007	-0.00007	0.24864	0.24421	0.00000
3/4y	0.19171	-0.19072	0.00000	0.00000	-0.00300	-0.00322	0.28317	-0.28666	0.00000
3/5y	0.19171	0.19072	0.00000	0.00000	0.00300	-0.00322	0.28317	0.28666	0.00000
4/6y	0.26854	-0.26886	0.00000	0.00000	-0.00567	-0.00608	0.02468	-0.02857	0.00000
4/7y	0.26854	0.26886	0.00000	0.00000	0.00567	-0.00608	0.02468	0.02857	0.00000
5/8y	0.31229	-0.31339	0.00000	0.00000	-0.00728	-0.00780	-0.26866	0.26893	0.00000
5/9y	0.31229	0.31339	0.00000	0.00000	0.00728	-0.00780	-0.26866	-0.26893	0.00000
1/1b	0.00000	0.00001	0.00000	0.00000	0.00005	0.00000	0.00000	0.00002	0.00000
2/2b	0.00043	-0.00039	0.00000	0.00000	0.01213	0.01210	0.00085	-0.00078	0.00000
2/3b	-0.00043	-0.00039	0.00000	0.00000	0.01213	-0.01210	-0.00085	-0.00078	0.00000
3/4b	0.00065	-0.00061	0.00000	0.00000	0.02632	0.02631	0.00056	-0.00052	0.00000
3/5b	-0.00065	-0.00061	0.00000	0.00000	0.02632	-0.02631	-0.00056	-0.00052	0.00000
4/6b	0.00080	-0.00075	0.00000	0.00000	0.03733	0.03733	-0.00021	0.00018	0.00000
4/7b	-0.00080	-0.00075	0.00000	0.00000	0.03733	-0.03733	0.00021	0.00018	0.00000
5/8b	0.00087	-0.00082	0.00000	0.00000	0.04351	0.04352	-0.00084	0.00078	0.00000
5/9b	-0.00087	-0.00082	0.00000	0.00000	0.04351	-0.04352	0.00084	0.00078	0.00000
Mxr%	0.000	0.000	63.392	0.000	0.000	0.000	0.000	0.000	7.454
Myr%	64.225	0.000	0.000	0.000	0.000	0.025	7.777	0.000	0.000
Mbr%	0.000	0.017	0.000	0.000	37.196	0.000	0.000	0.000	0.000

Mod	10.mod	11.mod	12.mod	13.mod	14.mod	15.mod	16.mod	17.mod	18.mod
w	39.39	48.58	48.54	66.87	67.38	68.04	68.15	84.43	84.37
T	0.1595	0.1294	0.1294	0.0940	0.0932	0.0924	0.0922	0.0744	0.0745
yön	x	y	b	y	b	x	x	y	b
1/1x	0.00000	0.00000	0.00000	0.00000	0.00000	0.00557	0.00000	0.00000	0.00000
2/2x	0.24202	0.00000	0.00000	0.00000	0.00000	0.31086	0.31090	0.00000	0.00000
2/3x	-0.24201	0.00000	0.00000	0.00000	0.00000	0.31086	-0.31090	0.00000	0.00000
3/4x	0.28856	0.00000	0.00000	0.00000	0.00000	-0.05782	-0.05571	0.00000	0.00000
3/5x	-0.28855	0.00000	0.00000	0.00000	0.00000	-0.05782	0.05571	0.00000	0.00000
4/6x	0.03014	0.00000	0.00000	0.00000	0.00000	-0.28178	-0.28244	0.00000	0.00000
4/7x	-0.03014	0.00000	0.00000	0.00000	0.00000	-0.28178	0.28244	0.00000	0.00000
5/8x	-0.26887	0.00000	0.00000	0.00000	0.00000	0.18871	0.18841	0.00000	0.00000
5/9x	0.26886	0.00000	0.00000	0.00000	0.00000	0.18871	-0.18841	0.00000	0.00000
1/1y	0.00000	0.00031	0.00000	0.01762	0.00000	0.00000	0.00000	0.00048	0.00000
2/2y	0.00000	-0.00082	-0.00082	0.30980	-0.31054	0.00000	0.00000	-0.00119	-0.00113
2/3y	0.00000	-0.00082	0.00082	0.30980	0.31053	0.00000	0.00000	-0.00119	0.00113
3/4y	0.00000	-0.00787	-0.00721	-0.06829	0.05924	0.00000	0.00000	-0.00665	-0.00593
3/5y	0.00000	-0.00787	0.00721	-0.06829	-0.05924	0.00000	0.00000	-0.00665	0.00593
4/6y	0.00000	-0.00366	-0.00333	-0.27889	0.28175	0.00000	0.00000	0.00845	0.00754
4/7y	0.00000	-0.00366	0.00333	-0.27889	-0.28175	0.00000	0.00000	0.00845	-0.00754
5/8y	0.00000	0.00635	0.00582	0.18995	-0.18880	0.00000	0.00000	-0.00370	-0.00330
5/9y	0.00000	0.00635	-0.00582	0.18995	0.18880	0.00000	0.00000	-0.00370	0.00330
1/1b	0.00000	0.00000	0.00015	0.00000	0.00004	0.00000	0.00000	0.00000	0.00026
2/2b	0.00000	0.03322	0.03327	0.00029	-0.00029	0.00000	0.00000	0.04310	0.04310
2/3b	0.00000	-0.03322	0.03328	-0.00029	-0.00029	0.00000	0.00000	-0.04310	0.04310
3/4b	0.00000	0.04015	0.04011	-0.00077	0.00068	0.00000	0.00000	-0.00716	-0.00727
3/5b	0.00000	-0.04015	0.04011	0.00077	-0.00068	0.00000	0.00000	-0.00716	-0.00727
4/6b	0.00000	0.00442	0.00438	-0.00055	0.00051	0.00000	0.00000	-0.03925	-0.03922
4/7b	0.00000	-0.00442	0.00438	0.00055	-0.00051	0.00000	0.00000	-0.03925	-0.03922
5/8b	0.00000	-0.03730	-0.03730	0.00067	-0.00060	0.00000	0.00000	0.02602	0.02603
5/9b	0.00000	0.03730	-0.03730	-0.00067	-0.00060	0.00000	0.00000	-0.02602	0.02603
Mxr%	0.000	0.000	0.000	0.000	0.000	2.403	0.000	0.000	0.000
Myr%	0.000	0.003	0.000	2.708	0.000	0.000	0.000	0.000	0.000
Mbr%	0.000	0.000	4.430	0.000	0.001	0.000	0.000	0.000	1.504

Mod	19.mod	20.mod	21.mod	22.mod	23.mod	24.mod	25.mod	26.mod	27.mod
w	93.04	93.39	93.67	93.75	116.81	116.77	192.43	322.09	351.38
T	0.0675	0.0673	0.0671	0.0670	0.0538	0.0538	0.0327	0.0195	0.0179
yön	y	b	x	x	y	b	y	x	b
1/1x	0.00000	0.00000	0.00533	0.00000	0.00000	0.00000	0.00000	0.38194	0.00000
2/2x	0.00000	0.00000	0.22645	0.22800	0.00000	0.00000	0.00000	-0.01002	0.00000
2/3x	0.00000	0.00000	0.22645	-0.22800	0.00000	0.00000	0.00000	-0.01002	0.00000
3/4x	0.00000	0.00000	-0.30429	-0.30409	0.00000	0.00000	0.00000	0.00211	0.00000
3/5x	0.00000	0.00000	-0.30430	0.30409	0.00000	0.00000	0.00000	0.00211	0.00000
4/6x	0.00000	0.00000	0.24967	0.24876	0.00000	0.00000	0.00000	-0.00034	0.00000
4/7x	0.00000	0.00000	0.24967	-0.24875	0.00000	0.00000	0.00000	-0.00034	0.00000
5/8x	0.00000	0.00000	-0.09369	-0.09325	0.00000	0.00000	0.00000	0.00001	0.00000
5/9x	0.00000	0.00000	-0.09370	0.09325	0.00000	0.00000	0.00000	0.00001	0.00000
1/1y	0.01810	0.00000	0.00000	0.00000	0.00038	0.00000	0.38106	0.00000	0.00000
2/2y	0.21837	-0.22558	0.00000	0.00000	-0.00280	-0.00250	-0.03195	0.00000	0.00097
2/3y	0.21837	0.22558	0.00000	0.00000	-0.00280	0.00250	-0.03195	0.00000	-0.00097
3/4y	-0.30535	0.30476	0.00000	0.00000	0.00128	0.00114	0.00870	0.00000	-0.00015
3/5y	-0.30535	-0.30476	0.00000	0.00000	0.00128	-0.00114	0.00870	0.00000	0.00015
4/6y	0.25377	-0.24989	0.00000	0.00000	-0.00060	-0.00053	-0.00200	0.00000	0.00002
4/7y	0.25378	0.24989	0.00000	0.00000	-0.00060	0.00053	-0.00200	0.00000	-0.00002
5/8y	-0.09555	0.09355	0.00000	0.00000	0.00017	0.00016	0.00025	0.00000	0.00004
5/9y	-0.09555	-0.09355	0.00000	0.00000	0.00017	-0.00016	0.00025	0.00000	-0.00004
1/1b	0.00000	0.00004	0.00000	0.00000	0.00000	0.00026	0.00000	0.00000	0.02790
2/2b	-0.00080	0.00070	0.00000	0.00000	0.03193	0.03185	-0.00012	0.00000	-0.00090
2/3b	0.00080	0.00070	0.00000	0.00000	-0.03193	0.03185	0.00012	0.00000	-0.00090
3/4b	-0.00024	0.00022	0.00000	0.00000	-0.04209	-0.04210	0.00004	0.00000	0.00021
3/5b	0.00024	0.00022	0.00000	0.00000	0.04209	-0.04210	-0.00004	0.00000	0.00021
4/6b	0.00092	-0.00081	0.00000	0.00000	0.03425	0.03430	-0.00001	0.00000	-0.00004
4/7b	-0.00092	-0.00081	0.00000	0.00000	-0.03425	0.03430	0.00001	0.00000	-0.00004
5/8b	-0.00050	0.00044	0.00000	0.00000	-0.01281	-0.01283	0.00001	0.00000	0.00000
5/9b	0.00050	0.00044	0.00000	0.00000	0.01281	-0.01283	-0.00001	0.00000	0.00000
Mxr%	0.000	0.000	0.628	0.000	0.000	0.000	0.000	26.123	0.000
Myr%	0.815	0.000	0.000	0.000	0.000	0.000	24.448	0.000	0.000
Mbr%	0.000	0.001	0.000	0.000	0.000	0.414	0.000	0.000	56.436

Mxr= $\sum[(\sum m_i \cdot \Phi)^2 / Mr] = \%100.00 > \%90.00$ Dinamik kütle oranı yeterli. ✓
Myr= $\sum[(\sum m_i \cdot \Phi)^2 / Mr] = \%100.00 > \%90.00$ Dinamik kütle oranı yeterli. ✓

EŞDEĞER DEPREM HESABI 1. DOĞAL TİTREŞİM PERİYODUNUN KONTROLÜ
N= 4.00 < 13

$\Sigma=100.0$
 $\Sigma=100.0$

YAPI BURULMA KÜTLE ATALET MOMENTİ $J_{mass}=(I_x+I_y)/A$

Kat	A (m ²)	I _x (m ⁴)	I _y (m ⁴)	X _g (m)	Y _g (m)	J _{mass} (m ²)
9	300.00	5625.00	10000.00	35.00	7.50	52.08
8	300.00	5625.00	10000.00	10.00	7.50	52.08
7	300.00	5625.00	10000.00	35.00	7.50	52.08
6	300.00	5625.00	10000.00	10.00	7.50	52.08
5	300.00	5625.00	10000.00	35.00	7.50	52.08
4	300.00	5625.00	10000.00	10.00	7.50	52.08
3	300.00	5625.00	10000.00	35.00	7.50	52.08
2	300.00	5625.00	10000.00	10.00	7.50	52.08
1	675.00	12656.25	113906.25	22.50	7.50	187.50

KAT KÜTLESİ ve RİJİTLİK MERKEZİ (t)

Kat (dyf)	H (m)	W _g	W _q	X _g (m)	X _r (m)	Y _g (m)	Y _r (m)	ΣW _k
5 (9)	15.00	214.52	60.00	35.00	35.00	7.50	7.50	232.524
5 (8)	15.00	214.52	60.00	10.00	10.00	7.50	7.50	232.524
4 (7)	12.00	214.52	60.00	35.00	35.00	7.50	7.50	232.524
4 (6)	12.00	214.52	60.00	10.00	10.00	7.50	7.50	232.524
3 (5)	9.00	214.52	60.00	35.00	35.00	7.50	7.50	232.524
3 (4)	9.00	214.52	60.00	10.00	10.00	7.50	7.50	232.524
2 (3)	6.00	214.52	60.00	35.00	35.00	7.50	7.50	232.524
2 (2)	6.00	214.52	60.00	10.00	10.00	7.50	7.50	232.524
1 (1)	3.00	644.66	135.00	22.50	22.50	7.50	7.50	685.160

ΣW_t = 2545.353

EŞDEĞER DEPREM FORMÜLÜ

$$F_{di} = (V_t - F_t) \frac{W_i \cdot H_i}{\sum W_i \cdot H_i}$$

DEPREM KUVVETİ (t)

Deprem tepe yükü $F_{tx} = 8.71$ $F_{ty} = 8.51$ (t)

X YÖNÜ

Y YÖNÜ

Kat no	Modal Analiz	Eşdeğer dep.yön.	Deprem yükü	Kat tipi	Modal Analiz	Eşdeğer dep.yön.	Deprem yükü	Kat tipi
5 (9)	27.018	33.714	27.583	UST KAT	26.713	32.960	26.977	UST KAT
5 (8)	27.018	33.714	27.583	UST KAT	26.713	32.960	26.977	UST KAT
4 (7)	19.526	22.020	19.934	NORMAL	19.071	21.527	19.259	NORMAL
4 (6)	19.526	22.020	19.934	NORMAL	19.071	21.527	19.259	NORMAL
3 (5)	14.007	14.680	14.299	NORMAL	13.774	14.351	13.911	NORMAL
3 (4)	14.007	14.680	14.299	NORMAL	13.774	14.351	13.911	NORMAL
2 (3)	7.995	7.340	8.162	NORMAL	8.185	7.176	8.266	NORMAL
2 (2)	7.995	7.340	8.162	NORMAL	8.185	7.176	8.266	NORMAL
1 (1)	74.316	182.709	74.316	BODRUM	57.649	182.709	57.649	BODRUM
Σ	211.406	338.217	214.273	GENEL	193.134	334.738	194.475	GENEL
	74.316	182.709	74.316	BODRUM	57.649	182.709	57.649	BODRUM
	137.090	155.507	139.957	NORMAL	135.484	152.028	136.826	NORMAL

$$V_{tx} = W \cdot A(t) / R_a(t) > 0,10 \cdot A_o \cdot I \cdot W = 155.51 > 74.41$$

$$V_{ty} = W \cdot A(t) / R_a(t) > 0,10 \cdot A_o \cdot I \cdot W = 152.03 > 74.41$$

$$X \text{ Deprem kontrol: } 0.90 \times 155.507 = 139.957 > 137.090 >>> 139.957$$

$$Y \text{ Deprem kontrol: } 0.90 \times 152.028 = 136.826 > 135.484 >>> 136.826$$

KİRİŞ VE KOLON KAPASİTELERİNE GÖRE YAPI GÖÇME YÜKÜ

KOLON TABAN KAPASİTE MOMENTLERİ TOPLAMI : $M_{rx} = 375.2$ (tm) $M_{ry} = 374.89$ (tm)KOLONLARA BAĞLI KİRİŞ KAPASİTE MOMENTLERİ TOPLAMI : $M_{rx} = 2193.28$ (tm) $M_{ry} = 2117.34$ (tm) $\sum M_c < \sum M_b > M_b = M_c$ KİRİŞ KAPASİTE MOMENTLERİ TOPLAMI : $M_{rx} = 2193.28$ (tm) $M_{ry} = 2117.34$ (tm)X YÖNÜ GÖÇME KAPASİTESİ : $P_x = 139.96 \times (375.2 + 2193.28) / 1241.36 = 250.15$ (t)Y YÖNÜ GÖÇME KAPASİTESİ : $P_y = 136.83 \times (374.89 + 2117.34) / 1210.64 = 249.93$ (t)ZAYIF KAT GÖÇME KAPASİTESİ: $P_x = 250.15$ (t), $P_y = 249.93$ (t)

Analiz sonuçlarındaki donatılara göre kapasite kontrol

 $V_{tx} = \lambda \cdot A_o \cdot I \cdot S(t) \cdot W = 951.7$ (t) ($\lambda = 0.85$) $V_{ty} = \lambda \cdot A_o \cdot I \cdot S(t) \cdot W = 930.41$ (t) ($\lambda = 0.85$)

X YÖNÜ

Y YÖNÜ

Kat no	Kolon ΣM _c	Kiriş (M _{ci} ≥ M _{bi}) ΣM _{bi}	Kapasite V _r	Kolon ΣM _c	Kiriş (M _{ci} ≥ M _{bi}) ΣM _{bi}	Kapasite V _r
5 (9)	281.26	447.46	187.51	281.26	419.09	187.51
5 (8)	320.37	703.93	213.58	320.24	670.14	213.49
4 (7)	320.37	962.69	213.60	320.24	921.19	213.49
4 (6)	351.81	1265.36	234.61	351.28	1214.29	234.19
3 (5)	351.81	1571.42	234.54	351.28	1507.39	234.19
3 (4)	375.22	1881.33	250.13	374.89	1812.37	249.93
2 (3)	375.20	2193.29	250.15	374.89	2117.34	249.93
2 (2)	375.20	2193.29	250.15	374.89	2117.34	249.93

(Mci ≥ Mbi) >> ∑Mbi Kiriş Plastik Mafsalsal Kontrolu

Rüzgar kuvvetleri (t)

Kat (dyf)	X-yönü F	X-yönü ey m	Y-yönü F	Y-yönü ex m
5 (9)	4.320	35.000	5.760	7.500
5 (8)	4.320	10.000	5.760	7.500
4 (7)	4.320	35.000	5.760	7.500
4 (6)	4.320	10.000	5.760	7.500
3 (5)	2.700	35.000	3.600	7.500
3 (4)	2.700	10.000	3.600	7.500
2 (3)	2.700	35.000	3.600	7.500
2 (2)	2.700	10.000	3.600	7.500
1 (1)	0.000	22.500	0.000	7.500

Kat Deprem deplasmanları

Kat (dyf)	9. yükleme		10. yükleme		11. yükleme		12. yükleme	
	δx (m)	θz (rad)	δx (m)	θz (rad)	δy (m)	θz (rad)	δy (m)	θz (rad)
5 (9)	0.0067477	0.0000640	0.0067477	-0.000064	-0.006945	-0.000076	-0.006956	0.0000897
5 (8)	0.0067477	0.0000640	0.0067477	-0.000064	-0.006956	-0.000089	-0.006945	0.0000768
4 (7)	0.0057417	0.0000545	0.0057417	-0.000054	-0.005921	-0.000064	-0.005932	0.0000773
4 (6)	0.0057417	0.0000545	0.0057417	-0.000054	-0.005932	-0.000077	-0.005921	0.0000643
3 (5)	0.0040506	0.0000383	0.0040506	-0.000038	-0.004215	-0.000043	-0.004226	0.0000563
3 (4)	0.0040506	0.0000383	0.0040506	-0.000038	-0.004226	-0.000056	-0.004215	0.0000434
2 (3)	0.0019052	0.0000177	0.0019052	-0.000017	-0.002048	-0.000017	-0.002058	0.0000289
2 (2)	0.0019052	0.0000177	0.0019052	-0.000017	-0.002058	-0.000028	-0.002048	0.0000174
1 (1)	0.0000323	0.0000001	0.0000323	-0.000000	-0.000091	-0.000000	-0.000091	0.0000002

Deprem yapı salınımları: x= 0.00045 y= 0.00046
Yapıda Deprem Perdeleri bulunamadı.

DEPREMDE YAPI DÜZENSİZLİKLERİNİN KONTROLU

A1,B2 düzensizliklerinin kontrolu

max(di/hi)=0.02

1. kat X dust = -.0000323 + -.0000001 x (.0 - 7.5) = -.0000316 (S101)
1. kat X dalt = -.0000323 + -.0000001 x (15.0 - 7.5) = -.0000331 (S131)
2. kat X dust = -.0019052 + -.0000177 x (.0 - 7.5) = -.0017406 (S201)
2. kat X dalt = -.0019052 + -.0000177 x (15.0 - 7.5) = -.0020051 (S231)

X YÖNÜ (+%5)

Kat	ΔX düst (m)	ΔX dalt (m)	ΔX ort	nbi	nki	ΔX/h	θi	kat tipi
5 (9)	0.0009344	0.0010776	0.0010060	1.07	0.00	0.00287	0.00283	Normal kat
5 (8)	0.0009344	0.0010776	0.0010060	1.07	0.00	0.00287	0.00141	Normal kat
4 (7)	0.0015698	0.0018124	0.0016911	1.07	1.68	0.00483	0.00349	Normal kat
4 (6)	0.0015698	0.0018124	0.0016911	1.07	1.68	0.00483	0.00276	Normal kat
3 (5)	0.0019914	0.0022995	0.0021455	1.07	1.27	0.00613	0.00456	Normal kat
3 (4)	0.0019914	0.0022995	0.0021455	1.07	1.27	0.00613	0.00404	Normal kat
2 (3)	0.0017406	0.0020051	0.0018729	1.07	0.87	0.00535	0.00441	Normal kat
2 (2)	0.0017406	0.0020051	0.0018729	1.07	0.87	0.00535	0.00415	Normal kat
1 (1)	0.0000316	0.0000331	0.0000323	1.02	0.00	0.00009	0.00000	Bodrum kat

X YÖNÜ (-%5)

Kat	ΔX düst (m)	ΔX dalt (m)	ΔX ort	nbi	nki	ΔX/h	θi	kat tipi
5 (9)	0.0010776	0.0009344	0.0010060	1.07	0.00	0.00287	0.00283	Normal kat
5 (8)	0.0010776	0.0009344	0.0010060	1.07	0.00	0.00287	0.00141	Normal kat
4 (7)	0.0018124	0.0015698	0.0016911	1.07	1.68	0.00483	0.00349	Normal kat
4 (6)	0.0018124	0.0015698	0.0016911	1.07	1.68	0.00483	0.00276	Normal kat
3 (5)	0.0022995	0.0019914	0.0021455	1.07	1.27	0.00613	0.00456	Normal kat
3 (4)	0.0022995	0.0019914	0.0021455	1.07	1.27	0.00613	0.00404	Normal kat
2 (3)	0.0020051	0.0017406	0.0018729	1.07	0.87	0.00535	0.00441	Normal kat
2 (2)	0.0020051	0.0017406	0.0018729	1.07	0.87	0.00535	0.00415	Normal kat
1 (1)	0.0000331	0.0000316	0.0000323	1.02	0.00	0.00009	0.00000	Bodrum kat

Y YÖNÜ (+%5)

Kat	ΔY dsol (m)	ΔY dsağ (m)	ΔY ort	nbi	nki	$\Delta Y/h$	θ_i	kat tipi
5 (9)	0.0008997	0.0011487	0.0010242	1.12	0.00	0.00306	0.00294	Normal kat
5 (8)	0.0009001	0.0011483	0.0010242	1.12	0.00	0.00306	0.00147	Normal kat
4 (7)	0.0014970	0.0019160	0.0017065	1.12	1.67	0.00511	0.00361	Normal kat
4 (6)	0.0014961	0.0019171	0.0017066	1.12	1.67	0.00511	0.00286	Normal kat
3 (5)	0.0019070	0.0024258	0.0021664	1.12	1.27	0.00647	0.00474	Normal kat
3 (4)	0.0018936	0.0024417	0.0021676	1.13	1.27	0.00651	0.00419	Normal kat
2 (3)	0.0017827	0.0021276	0.0019552	1.09	0.90	0.00567	0.00472	Normal kat
2 (2)	0.0016820	0.0022560	0.0019690	1.15	0.91	0.00602	0.00446	Normal kat
1 (1)	0.0000878	0.0000953	0.0000915	1.04	0.00	0.00025	0.00000	Bodrum kat

Y YÖNÜ (-%5)

Kat	ΔY dsol (m)	ΔY dsağ (m)	ΔY ort	nbi	nki	$\Delta Y/h$	θ_i	kat tipi
5 (9)	0.0011483	0.0009001	0.0010242	1.12	0.00	0.00306	0.00294	Normal kat
5 (8)	0.0011487	0.0008997	0.0010242	1.12	0.00	0.00306	0.00147	Normal kat
4 (7)	0.0019171	0.0014961	0.0017066	1.12	1.67	0.00511	0.00361	Normal kat
4 (6)	0.0019160	0.0014970	0.0017065	1.12	1.67	0.00511	0.00286	Normal kat
3 (5)	0.0024417	0.0018936	0.0021676	1.13	1.27	0.00651	0.00474	Normal kat
3 (4)	0.0024258	0.0019070	0.0021664	1.12	1.27	0.00647	0.00419	Normal kat
2 (3)	0.0022560	0.0016820	0.0019690	1.15	0.91	0.00602	0.00446	Normal kat
2 (2)	0.0021276	0.0017827	0.0019552	1.09	0.90	0.00567	0.00443	Normal kat
1 (1)	0.0000953	0.0000878	0.0000915	1.04	0.00	0.00025	0.00000	Bodrum kat

TDY 2.3.2.1 A1 burulma düzensizliği:

nbi=1.146 < 1.2 , dinamik analizle çözülmüştür ✓

TDY 2.3.2.1 B2 düzensizliği sağlanmaktadır. ✓

TDY 2.19 kosulu sağlanmaktadır. .0065 < .02 ✓

TDY 2.20 koşulu sağlanmaktadır. max θ_i =.005 < 0.12 ✓

B1-Düşey doğrultudaki düzensizliklerinin kontrolü

Kat	Aw	Agx	Agy	ΣA_{ex}	ΣA_{ey}	ncix	nciy	AÇIKLAMA
5	6.40	0.00	0.00	6.40	6.40	1.00	1.00	üst kat ✓
4	6.40	0.00	0.00	6.40	6.40	1.00	1.00	Düzenli ✓
3	6.40	0.00	0.00	6.40	6.40	1.00	1.00	Düzenli ✓
2	6.40	0.00	0.00	6.40	6.40	1.00	1.00	Düzenli ✓
1	2.56	25.06	8.78	27.62	11.34	4.32	1.77	bodrum kat

TDY A4 düzensizliği :

A4 düzensizliği bulunmamıştır. ✓